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ON THE CHERNOUS'KO TIME-OPTIMAL PROBLEM FOR THE EQUATION OF HEAT CONDUCTIVITY IN A ROD^{[1](#page-0-0)}

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Abstract: The time-optimal problem for the controllable equation of heat conductivity in a rod is considered. By means of the Fourier expansion, the problem reduced to a countable system of one-dimensional control systems with a combined constraint joining control parameters in one relation. In order to improve the time of a suboptimal control constructed by F.L. Chernous'ko, a method of grouping coupled terms of the Fourier expansion of a control function is applied, and a synthesis of the improved suboptimal control is obtained in an explicit form.

Keywords: Heat equation, Time-optimal problem, Pontryagin maximum principle, Suboptimal control, Synthesis of control.

Introduction

It is known that a time-optimal problem occupied a very important place in the foundation and development of optimal control theory. Even for simple non-trivial cases, the problem required working-out new approaches and lead after all to Pontryagin's maximum principle [\[3,](#page-9-0) [10,](#page-9-1) [30\]](#page-10-0). Despite 70 years of development, the solution of concrete non-trivial examples of time-optimal control still needs considerable effort [\[2,](#page-8-0) [4,](#page-9-2) [19\]](#page-9-3). The problem becomes even more difficult when a control system is described by a partial differential equation [\[11,](#page-9-4) [24,](#page-9-5) [25,](#page-9-6) [34\]](#page-10-1), particularly, for the heat conductivity equation [\[12,](#page-9-7) [22,](#page-9-8) [26,](#page-9-9) [29,](#page-10-2) [35,](#page-10-3) [36\]](#page-10-4). In [\[1\]](#page-8-1), the correctness of parabolic equations for heat propagation is discussed and for that purpose, a parabolic equation with time delay is considered.

Here, the maximum principle can be formally written out as well, but it loses its effectiveness as compared with a finite-dimensional case or on cases when the time interval is fixed [\[2,](#page-8-0) [9,](#page-9-10) [18,](#page-9-11) [25,](#page-9-6) [32,](#page-10-5) [33\]](#page-10-6). Therefore, Chernous'ko suggested [\[13\]](#page-9-12) another approach based on the Fourier expansion that allowed him to reduce the problem to an infinite system of one-dimensional problems whose control parameters are connected by a condition in the min-max form (see below (1.4)) generating a closed convex control set in a Hilbert space. Unfortunately, to deal with such a constraint is quite difficult (about other kinds of constraints see [\[17\]](#page-9-13)). In order to overcome this complexity, the mentioned constraint was replaced [\[13\]](#page-9-12) by an infinite system of separated conditions for scalar control parameters that can be interpreted as if one took Hilbert's brick inscribed into the control set. As a result, this approach made it possible to construct a suboptimal control and to give an explicit upper estimation for an optimal time. In [\[5\]](#page-9-14), a co-Hilbert's brick inscribed into the control set was considered, and an improved suboptimal control function was constructed. In the present

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paper, we suggest another way for constructing a suboptimal control function in the case of the heat conductivity equation in a rod.

1. Preliminaries

As it was noted above, Chernous'ko considered the time-optimal problem for an evolutional equation

$$
\frac{\partial u(t,x)}{\partial t} = A[u(\cdot,\cdot)](t,x) + v(t,x)
$$
\n(1.1)

with the initial and boundary conditions

$$
u(0,x) = u^{0}(x), \quad Mu(t,s) = u^{*}(t,s), \tag{1.2}
$$

where A is a uniformly elliptic differential operator, $t \geq 0$, $x \in D$, D is a regular domain with Lyapunov boundary Γ, $s \in \Gamma$, and M is a boundary operator [\[13\]](#page-9-12).

The constraint on the control function in problem (1.1) , (1.2) is bounded in the norm of the space L_{∞} ; i.e. $|v(t,x)| \leq v_0$ for almost all t and every $x \in \overline{D}$, where v_0 is a given positive number [\[31\]](#page-10-7). It is known that, for every control function $v(t, x)$, problem [\(1.1\)](#page-1-1), [\(1.2\)](#page-1-2) has a unique solution $u(t, x)$ [\[14,](#page-9-15) [21,](#page-9-16) [28\]](#page-10-8).

If a solution $u(t, x)$ of problem [\(1.1\)](#page-1-1), [\(1.2\)](#page-1-2) satisfies the condition $u(T, x) \equiv 0$ at some T, $T \ge 0$, then the corresponding control function $v(t, x)$ is called admissible, and the number T is called the transition time (from the initial state $u_0(\cdot)$ into the equilibrium state $u(t, x) \equiv 0$). Let V be the class of all admissible controls. Then the quantity $T = T[v(\cdot, \cdot)]$ will be a functional on V at every fixed $u^0(x)$ and $u^*(t, s)$.

If an admissible control $v_*(t, x)$ satisfies the condition $T_* = T[v_*(\cdot, \cdot)] \leq T[v(\cdot, \cdot)]$ for all $v(\cdot, \cdot) \in V$, then $v_*(\cdot, \cdot)$ is called a time-optimal control, and the value T_* is called optimal transition time.

The direct application of the Pontryagin maximum principle to problem (1.1) , (1.2) is a very hard task, unlike optimization problems on a finite interval of time (see $[4, 8, 15]$ $[4, 8, 15]$ $[4, 8, 15]$ $[4, 8, 15]$). For example, in [\[25\]](#page-9-6), only theorems on the existence of optimal control and the bang-bang principle are given, but no specific example of a solution was considered. In monograph [\[11\]](#page-9-4), the time-optimal problem when a control parameter participates in boundary conditions was considered [\[11,](#page-9-4) Ch. 5, Sect. 1] and, instead of the necessary conditions, the method of the L-momentum of N.N. Krasovskii [\[19\]](#page-9-3) was applied [\[11,](#page-9-4) Sect. 2]. In the recently published article [\[20\]](#page-9-19), Butkovsky's approach was applied to the case of a fractional-order diffusion equation. It should be noted that the L-momentum method only allows one to simplify to some degree the time-optimal problem and rarely gives an explicit solution. Therefore, the approach suggested by Chernous'ko [\[13\]](#page-9-12), where the method of expansions on the system of eigenfunctions of the operator A was used, seems to be more effective. That helped to reduce considering problem to the infinite system of one-dimensional control problems:

$$
\dot{y}_k = -\lambda_k y_k + v_k, \quad y_k(0) = y_{k0}, \quad k = 0, 1, 2, \dots \,.
$$
 (1.3)

(About solution of systems of this kind, see $[16]$).

In terms of system [\(1.3\)](#page-1-3), the condition $|v(t, s)| \le v_0$ means that a counting system of the control parameters v_k , $k = 0, 1, 2, \ldots$, should satisfy the combined constraint

$$
\max_{x \in \overline{D}} \left| \sum_{k=0}^{\infty} \varphi_k(x) v_k \right| \le v_0. \tag{1.4}
$$

where φ_k are eigenfunctions of the problem.

Condition [\(1.4\)](#page-1-0) defines some closed convex set L in the Hilbert space l_2 , which is difficult to deal with. In this connection, it is natural to try to solve the problem of finding a suboptimal control. (It is essential to note that, if a time interval is fixed, then the method of penalty functions is enough effective for the construction of a suboptimal control. It would be interesting to apply this method for the time-interval problem as well $[6]$.) For this purpose, in [\[13\]](#page-9-12), constraint (1.4) was replaced by a more rigid system of constraints in the form

$$
|v_k| \le U_k, \quad k = 0, 1, 2, \dots,
$$
\n^(1.5)

where $\alpha_k = \max_{x \in \overline{D}} |\varphi_k(x)|$. Wherein, nonnegative numbers U_k should be chosen satisfying the con $x\in\bar{D}$ dition $\sum_{k=0}^{\alpha} \alpha_k U_k = v_0$.

Let T_{*k} be an optimal transition time in the problem

$$
\dot{y}_k = -\lambda_k y_k + v_k, \quad y_k(0) = y_k^0,
$$
\n(1.6)

such that $y_k(T_{*k}) = 0, k = 0, 1, 2...$ In [\[13\]](#page-9-12), it is shown that the numbers U_k can be chosen so that all T_{*k} coincide: $T_{*k} = T$ for some \hat{T} . Let $\hat{v}_k(t)$ be the sequence of the corresponding optimal controls. Then $T_* \leq \hat{T}$ and $\hat{v}_*(t,x) = \sum_{k=0}^{\infty} \varphi_k(x) v_{*k}(t)$ may serve as the sought suboptimal control.

A new problem arises here: is it possible to use a more exact reduction of the constraint than (1.5) ? As mentioned above in $[5]$ it was used Hilbert's co-cube instead of (1.5) . Here, we are going to follow another approach based on a special grouping of terms of [\(1.5\)](#page-2-0). Effectiveness of this approach is tightly related to specific properties of eigenfunctions $\varphi_k(\cdot)$, so here it will be demonstrated for the operator $A = \frac{\partial^2}{\partial x^2}$ connected with the process of the heat conductivity in a rod.

2. A method of grouping terms of the Fourier expansion

Consider the following concretization of problem [\(1.1\)](#page-1-1), [\(1.2\)](#page-1-2):

$$
\begin{cases}\n\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} + v(t, x), & |v(t, x)| \le v_0, \quad t \ge 0, \quad 0 \le x \le \pi, \\
u(0, x) = u^0(x), & u(t, 0) = 0, \quad u(t, \pi) = 0.\n\end{cases}
$$
\n(2.1)

The system of eigenfunctions $\varphi_k(t) = \sin kx$, $k = 1, 2, \dots$, of the operator $\partial^2/\partial x^2$ forms a complete orthogonal basis of the space $L_2[0, \pi]$ [\[21,](#page-9-16) [28\]](#page-10-8).

Let $u(t,x) = \sum_{k=1}^{\infty} y_k \sin kx$ and $v(t,x) = \sum_{k=1}^{\infty} v_k \sin kx$ be the Fourier expansions on the basis $\{\sin kx\}$. Then the restriction [\(1.4\)](#page-1-0) takes the form

$$
\max_{0 \le x \le \pi} \left| \sum_{k=1}^{\infty} v_k \sin kx \right| \le v_0. \tag{2.2}
$$

Let us consider a more rigid restriction

$$
\max_{0 \le x \le \pi} \sum_{k \in Q} \left| v_k \sin kx + v_{3k} \sin 3kx \right| \le v_0 \tag{2.3}
$$

instead of [\(2.2\)](#page-2-1), thereby replacing the optimal control problem with a suboptimal control problem. System [\(1.6\)](#page-2-2) takes the form

$$
\dot{y}_k = -k^2 y_k + v_k, \quad k \in \mathbb{Z}^+.
$$
\n(2.4)

Let Q be the set of all positive integers having the form $3^{2p}q$, where $p = 0, 1, 2, \ldots$, and q is relatively prime with 3. It is obvious that the set of all positive integers Z^+ is the union of the two disjoint sets Q and $3Q$. Then (2.4) can be rewritten in the form

$$
\dot{y}_k = -k^2 y_k + v_k, \quad \dot{y}_{3k} = -9k^2 y_{3k} + v_{3k}, \quad k \in Q.
$$
 (2.5)

After the substitutions

$$
y_k = \frac{\mu_k}{k^2} x^1
$$
, $y_{3k} = \frac{\mu_k}{k^2} x^2$, $t = \frac{1}{k^2} \tau$, $v_k = \mu_k w^1$, $v_{3k} = \mu_k w^2$,

all systems [\(2.5\)](#page-3-0) will be reformulated to the following two-dimensional control system:

$$
\dot{x}^1 = -x^1 + w^1, \quad \dot{x}^2 = -9x^2 + w^2.
$$
\n(2.6)

Now, following the Chernous'ko way, we replace [\(2.3\)](#page-2-4) by the even more rigid restriction

$$
\max_{0 \le x \le \pi} \left| w_k^1 \sin kx + w_k^2 \sin 3kx \right| \le 1, \quad k \in Q,\tag{2.7}
$$

that implies [\(2.3\)](#page-2-4) if $\sum_{k\in Q}\mu_k=v_0$. Thus, we have reduced the infinite dimensional control problem to the two-dimensional problem.

3. Solution of the auxiliary time-optimal problem on the plane

Let P_k denote the set of all pairs (w_k^1, w_k^2) for which (2.7) holds. Setting

$$
P = \left\{ w = (w^1, w^2) \in R^2 : \max_{0 \le t \le \pi} |w^1 \sin t + w^2 \sin 3t| \le 1 \right\},\
$$

we have $P_k = \mu_k P$. As a result, the considered problem of constructing a suboptimal control reduces to the concrete problem of time-optimal control for the following two-dimensional system:

$$
\dot{x}^1 = -x^1 + w^1, \quad \dot{x}^2 = -9x^2 + w^2, \quad (w^1, w^2) \in P. \tag{3.1}
$$

Obviously, P is a convex and compact set with non-empty interior (i.e., a convex body). Since P is symmetric with respect to the origin, we may restrict ourselves to considering only the case $w^1 \geq 0$. It is more convenient to set sin $t = y$. Then, by the formula

$$
\sin 3t = 3\sin t - 4\sin^3 t,
$$

we get

$$
P = \left\{ w = (w^1, w^2) \in R^2 : \max_{0 \le y \le 1} \left| (w^1 + 3w^2) y - 4w^2 y^3 \right| \le 1 \right\}.
$$

Just this transformation lay on the base of the separation $Z^+ = Q \cup 3Q$.

After elementary calculations, we find that the part of the boundary of the set P lying in the half-plane $w^1 \geq 0$ is given by the formula

$$
w^{1} = \begin{cases} w^{2} + 1 & \text{if } -1 \leq w^{2} < 0.125, \\ 3(\sqrt[3]{w^{2}} - w^{2}) & \text{if } 0.125 \leq w^{2} \leq 1, \end{cases}
$$

while the other part is found by central symmetry (see Fig. [1\)](#page-4-0).

Let us recall that, in the auxiliary problem (3.1) , a unique optimal time-control function exists at each initial point (x_0^1, x_0^2) [\[7,](#page-9-22) [23,](#page-9-23) [27\]](#page-10-9). The existence follows from the property $O \in \text{Int } P$. The

Figure 1. The straight ray AC is tangent at the point A to the curve AD, which is a part of the boundary of P.

uniqueness is a consequence of the following feature of P : the vector $(1,1)$, which is orthogonal to the segment AC , is not an eigenvector of the matrix of system (3.1) . Therefore, the optimal control problem [\(2.5\)](#page-3-0) coincides with the extremal controls of Pontryagin's maximum principle [\[23,](#page-9-23) [30\]](#page-10-0).

To calculate the latter, we prefer to use the "backward motion" principle. Let $T(x_0^1, x_0^2)$ be a transition time for the initial point (x_0^1, x_0^2) in the system [\(3.1\)](#page-3-2). If we set $\tau = T(x_0^1, x_0^2) - t$, then extremals of Pontryagin's maximum principle are defined by the system

$$
\begin{cases}\n\frac{dx^1}{d\tau} = x^1 - \bar{w}^1, & \frac{dx^2}{d\tau} = 9x^2 - \bar{w}^2, \\
x(0) = y(0) = 0, & \psi_1(0) = \cos s, \\
\psi_2(0) = \sin s, & -\pi \le s \le \pi.\n\end{cases}
$$
\n(3.2)

Since $\psi_1(\tau, s) = e^{-\tau} \cos s$ and $\psi_2(\tau, s) = e^{-9\tau} \sin s$, an extremal control $\bar{w}(\tau, s)$ should be found by the Pontryagin's maximum principle, i.e., from the equation

$$
\bar{w}^1(\tau,s)e^{-\tau}\cos s + \bar{w}^2(\tau,s)e^{-9\tau}\sin s = \max_{w \in P} [w^1e^{-\tau}\cos s + w^2e^{-9\tau}\sin s].\tag{3.3}
$$

Equation [\(3.3\)](#page-4-1) leads to the following construction of the extremal controls.

If $\psi(\tau, s)$ lies in the open angle AOB, then obviously $\bar{w}(\tau, s) = (0, 1)$. Note that, if $s = \pi/2$, then $\psi_1(\tau, s) \equiv 0$. Therefore, $\bar{w}(\tau, \pi/2) = (0, 1)$. Similarly, if $s = 0$, then $\psi_2(\tau, s) \equiv 0$; thus, $\bar{w}(\tau,0) = (2\sqrt{3}/3, \sqrt{3}/9).$

Consider now the dynamics of $\psi(\tau, s)$. In the case $0 < s < \pi/2$, the vector $\psi(\tau, s)$ lies in the quarter $\psi_1 > 0$, $\psi_2 > 0$ and turns clockwise. Moreover, its direction tends to the axis of abscissas OE as $\tau \to +\infty$. (Similarly, if $-\pi/2 < s < 0$, then $\psi(\tau, s)$ lies in the quarter $\psi_1 > 0$, ψ_2 < 0 and turns counterclockwise with the same limit direction.)

Thus, the extremal control has the following structure: if $0 < s \leq \arctan 2$ (see Fig. [1\)](#page-4-0), then $\psi(\tau, s)$ lies in the angle BOD for all $\tau (\tau \geq 0)$, and, hence, $\bar{w}(\tau, s)$ is a point of the arc AD such that its projection to the direction $\psi(\tau, s)$ is maximal (the analytical expression for $\bar{w}(\tau, s)$ is given in Table [1\)](#page-5-0).

	$\bar{w}^{\mu}(\tau,s)$	$\bar{w}^2(\tau,s)$
	0 if $0 \leq \tau \leq \tau_{**},$	-1 if $0 \leq \tau \leq \tau_{**}$,
$-\frac{\pi}{2} < s \leq -\frac{\pi}{4}$	$3(2 - e^{-8\tau} \tan s)M$ if $\tau_{**} \leq \tau$	M if $\tau_{**} \leq \tau$
$-\pi/4 < s < 0$	$3(2 - e^{-8\tau} \tan s) M$	
$s=0$	$2\sqrt{3}/3$	$\sqrt{3}/9$
$0 < s \leq \arctan 2$	$3(2 - e^{-8\tau} \tan s) M$	
π $\arctan 2 < s < \frac{1}{2}$	0 if $0 < \tau < \tau_*,$	1 if $0 \leq \tau \leq \tau_*$,
	$3(2-e^{-8\tau}\tan s)M$ if $\tau_* \leq \tau$	M if $\tau_* < \tau$
$s=\pi/2$		

Table 1. The analytical expression for $\bar{w}^1(\tau,s)$ and $\bar{w}^2(\tau,s)$.

Table 2. The analytical expression for $x^1(\tau, s)$ and $x^2(\tau, s)$.

	$x^1(\tau,s)$	$x^2(\tau,s)$
	0 if $0 \leq \tau \leq \tau_{**},$	$(e^{9\tau}-1)/9$ if $0 \leq \tau \leq \tau_{**},$
	$-\frac{\pi}{2} < s \leq -\frac{\pi}{4} \left \quad \frac{3e^{\tau}}{4\tan s} \int \frac{1-p^2}{p^2q^7} dp \quad \text{if} \quad \tau_{**} \leq \tau \right.$	$\frac{e^{9\tau}}{4\tan s}\int_{0}^{\pi}qdp \quad \text{if} \quad \tau_{**} \leq \tau$
$-\pi/4 < s < 0$	$\frac{3e^{\tau}}{4\tan s}\int \frac{1-p^2}{p^2q^7}dp$	$\frac{e^{9\tau}}{4\tan s}\int_{}^{n}qdp$
$s=0$	$\frac{2\sqrt{3}(1-e^{\tau})}{n}$	
$0 < s \leq \arctan 2$	$\frac{3e^{\tau}}{4\tan s}\int \frac{1-p^2}{p^2q^7}dp$	$\frac{\frac{m}{\sqrt{3}(1-e^{9\tau})/81}}{\frac{e^{9\tau}}{4\tan s}\int qdp}$
	0 if $0 \leq \tau \leq \tau_*,$	$\frac{m}{(1-e^{9\tau})/9}$ if $0 \leq \tau \leq \tau_*,$
	$\arctan 2{<}s{<}\frac{\pi}{2}\ \Bigg \ \frac{3e^{\tau}}{4\tan s}\int\limits^{\cdot}\frac{1-p^2}{p^2q^7}dp\quad \text{if}\quad \tau_*\leq\tau$	$\frac{e^{9\tau}}{4\tan s}\int_{0}^{n}qdp \quad \text{if} \quad \tau_{*} \leq \tau$
$s=\pi/2$		$\overline{(1-e^{9\tau})}/9$

Further, in the case arctan $2 < s < \pi/2$, we have $\bar{w}(\tau, s) = (0, 1)$ on the interval $[0, \tau_*)$, where $\tau_* = -1/8 \cdot \log(2 \cot s)$. At the time $\tau = \tau_*$, the vector $\psi(\tau, s)$ becomes orthogonal to the right side tangent to the curve ∂P at the point $(0,1)$ and it occurs "switching" of the extremal control from the value (0, 1) to a continuous mode. Namely, $\bar{w}(\tau, s)$ begins sliding along the arc AC (see Table [1\)](#page-5-0) and tends to the point C as $\tau \to +\infty$.

Similarly, if $(-\pi/2 < s < -\pi/4)$, then $\bar{w}(\tau, s) = (0, -1)$ at $0 \leq \tau < \tau_{**}$, where $\tau_{**} =$ $-1/8 \cdot \log(-\cot s)$ and $w(\tau, s)$ is a switching time. On the interval $(\tau_{**}, +\infty)$, $\bar{w}(\tau, s)$ slides along the arc ED tending to the point D.

The entire synthesis of the extremal control is given in Table [1.](#page-5-0) Due to the central symmetry, the values of s are considered only on the range $-\pi/2 < s \leq \pi/2$ and the following notation is used:

$$
M = (3 - e^{-8\tau} \tan s)^{-3/2}, \quad m = (3e^{8\tau} \cot s - 1)^{-1/2}, \quad n = (3 \cot s - 1)^{-1/2}
$$

$$
p = (3 - e^{-8\tau} \tan s)^{-1/2}, \quad q = ((3 - p^{-2}) \cot s)^{1/8}.
$$

,

Now, extremal trajectories can be easily calculated by [\(3.2\)](#page-4-2). The corresponding formulas are gathered in Table [2.](#page-5-1) They are illustrated in Fig. [2.](#page-6-0)

Figure 2. The extremal trajectories.

Figure 3. The graphs of the functions $\bar{w}^1(\tau,s)$ (the continuous line) and $\bar{w}^2(\tau,s)$ (the dashed line) for $\arctan 2 < s < \pi/2$.

4. Construction of a suboptimal control in the initial problem

Let us now derive the solution of problem (2.1) , (2.3) , (2.5) basing one of reduced problems. Extremals $x(t, s)$, $y(t, s)$ cover R^2 . Therefore, for every $(x_0^1, x_0^2) \in R^2 \setminus (0, 0)$, there exists a pair (τ_0, s_0) such that $x^1(\tau_0, s_0) = x_0^1$, $x^2(\tau_0, s_0) = x_0^2$. Further, in the system [\(3.1\)](#page-3-2), for every fixed $(x_0^1, x_0^2) \neq 0$, an optimal control is unique, which implies the uniqueness of the value τ_0 (while corresponding values of s_0 may be not unique, but one can choose any of them).

Then $T(x_0^1, x_0^2) = \tau_0$ is the transition time and

$$
\bar{v}^1(t) = v^1(\tau_0 - t, s_0), \quad \bar{v}^2(t) = v^2(\tau_0 - t, s_0)
$$

Figure 4. The graphs of the functions $\bar{w}^1(\tau,s)$ (the continuous line) and $\bar{w}^2(\tau,s)$ (the dashed line) for $-\pi/2 < s < \arctan 2$.

is the suboptimal control for [\(2.1\)](#page-2-5).

Let us now consider system [\(2.5\)](#page-3-0). For an initial point (y_k^0, y_{3k}^0) , the corresponding trajectory $(y_k(t), y_{3k}(t))$ satisfies the condition

$$
y_k(T_k) = y_{3k}(T_k) = 0,
$$

where

$$
T_k(\mu_k) = \frac{1}{k^2} \left(\frac{k^2}{\mu_k} y_k^0, \frac{k^2}{\mu_k} y_{3k}^0 \right).
$$

The constructed synthesis implies that T_k is monotonically decreasing in μ_k , and it is easy to see that $T_k \to 0$ as $\mu_k \to +\infty$ and $T_k \to \infty$ as $\mu_k \to 0$. Therefore, for every k, there exists a unique value μ_k^* such that $T_k(\mu_k^*)$ is the same for all k. Moreover, μ_k^* can be chosen satisfying the condition $\sum \mu_k^* = v_0$. One can easily see that

$$
\frac{\alpha}{k^2} \le \mu_k^* \le \frac{\beta}{k^2}
$$

for some positive α and β .

Finally, we consider the initial problem [\(2.1\)](#page-2-5), [\(2.3\)](#page-2-4), [\(2.5\)](#page-3-0). Let $u_0(x) = \sum_{k=1}^{\infty} u_k^0 \sin x$ be the Fourier expansion of the initial function $u_0(x)$. Taking (y_k^0, y_{3k}^0) , $k \in Q$, as an initial point for system [\(2.6\)](#page-3-3), we find

$$
\bar{w}_k^0(t) = \frac{1}{\mu_k} \bar{v}_k^1(t), \quad \bar{w}_{3k}^0(t) = \frac{1}{\mu_k} \bar{v}_k^2(t), \quad k \in Q.
$$

Thus, the following statement holds.

Theorem 1. The function

$$
\bar{v}(t,x) = \sum_{k=1}^{\infty} \bar{w}_k^0(t) \sin kx
$$

is a suboptimal control in problem (2.[1\)](#page-2-5) for the initial state $u_0(x)$.

5. Conclusion

The paper is devoted to the time-optimal problem for the process of heat conductivity in a rod when the control parameter is the intensity of external heat sources. A suboptimal control is constructed by the combination of the Chernous'ko approach with the method of grouping terms of the Fourier expansion.

This method may be applied to the time-optimal control problem for other systems given in an evolutionary form.

The following question naturally arises: how effective is the method of grouping? First of all, let us bring general considerations. The set of all admissible controls in the initial problem (1.1) – (1.2) can be identified with the subset

$$
U_{Initial} = \Big\{ u \in l_2 \mid \sup_{0 \le x \le \pi} |\sum_{k=0}^{\infty} u_k \sin kx| \le v_0 \Big\}.
$$

As noted in Section 1, Chernous'ko restricted the set of controls using

$$
U_{Ch} = \Big\{ u \in l_2 \mid |u_k| \le U_k, \ \ k = 1, 2, 3, \dots \Big\},\
$$

where U_k is a sequence chosen from the condition $\sum U_k \le v_0$ and guaranteeing the equality $u(t, x) \equiv 0$ for some $T = T_{Ch} > 0$.

The considerations in this paper are based on the set

$$
U_{gr} = \left\{ u \in l_2 \mid \max_{0 \le x \le \pi} |u_k \sin kx + u_{3kx} \sin 3kx| \le U_k \right\}
$$

taken as a region of admissible controls.

One can easily see that

$$
U_{gr} \subset U_{Ch} \subset U_{Initial}.
$$

These relations imply $T_2 \leq T_1 \leq T_0$ for optimal and suboptimal times of transition respectively.

If one takes an initial point of the form $(0,0,\ldots,x_m^0,0,\ldots,0)$, i.e., in terms of the initial problem (1.1) – (1.2) , $\varphi(x) = (0, 0, \ldots, x_m^0 \sin mx, 0, \ldots, 0)$, then, obviously, $U_{Initial} = U_{Ch} = U_{gr}$ and, thus, $T_2 = T_1 = T_0$. But if an initial point is taken in the form $(0, 0, \ldots, 0, x_k^0, 0, \ldots, 0, x_{3k}^0, 0, \ldots)$, then $U_{In}=U_{gr}$ while $U_{In}\supset U_{Ch}$ and, thus, $T_2=T_0 < T_1$. Table [3](#page-8-2) contains values for specific cases.

Obviously, $x_k^0 \neq 0$ at least for three values of the index k when $T_2 < T_0 < T_1$.

The final note is that the method of grouping can be applied only if there some algebraic relations between the eigenfunctions of the operator A.

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